

## Mathematical modelling of electrolysis processes

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The paper presents the optimization of sodium hypochlorite electrochemical production processes and zinc electroextraction by mathematical modeling method. On the basis of the model equations the values of the following parameters are defined – current density, components concentrations, duration for which there are maximum current efficiencies, minimum voltage and specific energy consumption. It is shown that the current efficiency maxima – ~70% for the platinized titanium anodes Pt/Ti – correspond to current densities  $7.5 \text{ A}\cdot\text{dm}^{-2}$ , and for the cobalt-oxide anodes  $\text{CoO}_x/\text{Ti}$  – 75% to current densities  $2.5 \text{ A}\cdot\text{dm}^{-2}$ . The highest values of the conversion coefficients (2.54%) are at low sodium chloride concentrations  $\sim 25 \text{ g}\cdot\text{dm}^{-3}$ . In case of increase in current densities up to  $10 \text{ A}\cdot\text{dm}^{-2}$ , the conversion coefficient could grow to 6%, but this leads to a considerable increase of energy consumption –  $25 \text{ W}\cdot\text{g}^{-1}$ .

In zinc electroextraction the lowest voltage  $\sim 3.1 \text{ V}$  is at current densities  $i = 200\text{--}300 \text{ A}\cdot\text{m}^{-2}$  and space between the opposite electrodes of 20–30 mm.

**Key words:** mathematical model, relation coefficient, binary oxides, electrosynthesis, electroextraction.

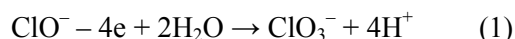
### INTRODUCTION

Sodium hypochlorite finds application as an antiseptic for the treatment of waste waters and aggressive solutions [1–3], in discolouration of pigment production wastes [4], etc.

The electrochemical method of its production has found application due to the advantages it possesses – clean product, low labour and chemicals consumptions, facilitated possibilities of automation and control. The method is based on the electrolysis of sodium chloride solutions; the hypochlorite production is a result of the interaction between the evolved on the anode and undergone hydrolysis chlorine and the formed on the cathode alkaline metal base.

Characteristic features of the considered process are the secondary reactions of chlorate formation and oxygen release, which lead to current efficiency decrease and specific electric energy consumption increase.

The reaction of sodium chlorate formation proceeds at more negative potentials than those of chlorine ions oxidation.

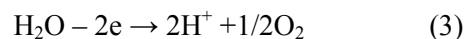


Moreover, chlorate is obtained also in the solution volume as a result of the oxidation effect of the hypochlorous acid formed during chlorine hydro-

lysis:



The oxygen evolution, on its part, at pH values at which the process goes  $\sim 5.5\text{--}7.5$  is a result of the oxidation of water molecules.



The occurrence of these reactions results in a decrease of the process current efficiency and increase in the electric energy consumption.

The optimization of these parameters appears currently the main problem of the sodium hypochlorite electrolysis; the correct selection of the electrolysis conditions – charge salt concentration, current densities, duration, the type of the anode material are the main factors in this respect .

Yang *et al.* [4, 5] investigate the production of sodium hypochlorite on the basis of Ru-Pt binary oxide anodes  $[(\text{Ru-Pt})\text{O}_x]$ , prepared by thermal method on titanium substrate.

At a current density  $300\text{--}500 \text{ mA}\cdot\text{cm}^{-2}$  and chlorine ion concentration of  $0.5\text{--}1.0 \text{ mol}\cdot\text{dm}^{-3}$  there are achieved current efficiency 80 – 85% and energy yield  $120\text{--}140 \text{ g}\cdot\text{kWh}^{-1}$ .

Kupovich *et al.* [6] investigate ferro-oxide titanium anodes containing mainly magnetite  $\text{Fe}_3\text{O}_4$ , small quantities of hematite  $\text{Fe}_2\text{O}_3$  and wustit  $\text{FeO}$ . The authors find out that the active mass retains stability in chlorine environment for 9 000–10 000 hours: modification by  $\text{CoO}$  (up to 35%), on its part,

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significantly improves the anode electrocatalytic properties.

A research on the sodium hypochlorite electro-synthesis on spinel coated electrodes is described in [7]. There are studied anodes – spinels of general formula  $AB_2O_4$ , where A is cobalt and B – cobalt, iron, chromium, aluminum. The experiments are performed at current densities 170–290  $\text{mA}\cdot\text{cm}^{-2}$  and sodium chloride concentration – 150  $\text{g}\cdot\text{dm}^{-3}$ . The authors find out that current efficiencies depend on the type of the spinel metal, decreasing in the sequence Al-Fe-Co-Cr.

Yang [8] proves the possibility to use Ru–Sn binary oxides  $[(\text{Ru}+\text{Sn})\text{O}_2]$  in the hypochlorite production by hydrolysis. The introduction of tin oxide in the anode active mass increases the overvoltage of oxygen  $\text{O}_2$  release and raises the current efficiency; in the current density range 100–150  $\text{mA}\cdot\text{cm}^{-2}$  and sodium chlorite concentration 0.5  $\text{m}\cdot\text{dm}^{-3}$  the presence of  $\text{SnO}_2$  to 20% increases current efficiency from 85 to 90–95 %.

Kraft *et al.* [9, 10] carry out comparative investigations of platinum anodes and iridium oxide coated titanium ones/ $\text{IrO}_2$ . It is found out that in diluted chloride solutions hydrolysis (250–1000  $\text{mg}\cdot\text{dm}^{-3}$ ) the rate of hypochlorite formation on titanium-iridium oxide anode is higher compared to that on platinum; at current density 15  $\text{mA}\cdot\text{cm}^{-2}$  the current efficiencies are 75 and 50%, respectively.

Sorokendia *et al.* [11] examine the NaClO electrolysis on palladium alloyed manganese dioxide anodes. The authors find out that in case of palladium oxide PdO content 1–2.5 mol.%, the current efficiencies have values about 85%, which are close to the current efficiencies of palladium oxide anodes ~ 90%.

In a number of publications there are studied the possibilities to optimize the process by using membranes. Publication [12] considers an inorganic membrane on the base of zirconium oxide/ $\text{ZrO}_2$ . It is proved that the final product does not contain chlorates.

As a result of that, higher current efficiencies reaching 77% with sodium chloride concentration 25  $\text{g}\cdot\text{dm}^{-3}$  and current density 6  $\text{mA}\cdot\text{cm}^{-2}$  are achieved on the used cobalt oxide/ $\text{Co}_3\text{O}_4$  anodes. Publications [13–16] also report about usage of membranes.

Zinc, together with aluminum and copper, is one of the widely used non-ferrous metals. Major method of its production is electroextraction due to which metal of high purity running up to 99.99% is obtained. The electrolysis is performed by insoluble anodes (lead alloyed with 1% silver), but in contrast to sodium hypochlorite production it is referred to

the so-called electrochemical processes with metal release. The hydrogen evolution is a basic secondary reaction; it is favoured by the circumstance that the used electrolytes contain sulphuric acid up to 100  $\text{g}\cdot\text{dm}^{-3}$ . The problems related to current efficiency and specific energy consumption present interest taking into account the large scale character of the electrolysis. They depend on the current density, components concentrations, the temperature and hydrodynamics. Some publications [17, 18] inform that every current density has a corresponding sulphuric acid concentration for which the process energy consumption is minimal.

Many authors use the mathematical modeling method in the electrolysis process optimization [19–23]. As it is well known, the mathematical models represent exact quantitative correlations between the input and output parameters of a system. Their development allows to calculate the values of the individual quantities in advance, to define their maximum or minimum values, to apply flexible approach in respect to the processes, etc.

The authors of publications [24–26] have shown the possibilities to apply models in the optimization of sodium hypochlorite electrochemical production process and zinc electroextraction. The present paper is a continuation of the researches in this aspect, its main purpose being development of mathematical model equations which connect current efficiencies and energy consumption with the electrolysis conditions – current density, duration, components concentrations, type of anode material.

## EXPERIMENTAL

In the NaClO production, the used anodes (dimensions 50×40×1 mm) were graphite,  $\text{CoO}_x$ , Pt-Ti and on the cathode – steel. The initial solutions were prepared of NaCl p.a. The electrolysis was carried out in a cell of volume 0.5 l without a diaphragm. The determination of the active chlorine quantity was performed by iodometry, by titration with 0.1 N  $\text{Na}_2\text{S}_2\text{O}_3$  solution in acidic environment. The temperature was maintained by a thermostat UTU-2 and for constant current intensity – potentiostat-galvanostat Tacussel 30-01.

The process quantitative characteristics were calculated on the basis of the Faraday's laws.

In the studies of zinc electroextraction process a PVC cell (0.5  $\text{dm}^3$ ) was used, which has rectangular shape permitting variation of the distance between the cathode and anode from 10 to 100 mm. The Zn concentration was 65  $\text{g}\cdot\text{dm}^{-3}$ . In the cell there are positioned three electrodes (dimensions 20×25×1 mm), 2 anodes (alloy, lead with 1% antimony) and 1 cathode (aluminum), respectively.

Voltage measurement was performed by means of a precise electron voltmeter 1AB105.

The processing of the results and development of mathematical models were performed by adequate computer program.

### RESULTS AND DISCUSSION

Figure 1 presents the diagram of the electrochemical process in mathematical modeling. In the Figure X and Y are independent factors – current density, electrolyte concentration – initial substance (time), and Z<sub>1</sub> and Z<sub>2</sub> – the functions or dependent factors – current efficiency and specific energy consumption (voltage).

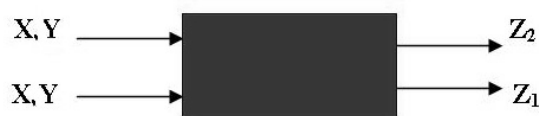


Fig. 1. Diagram of electrochemical system: X, Y – independent factors; Z<sub>1</sub>, Z<sub>2</sub> – dependent factors;

On the basis of preliminary experiments that show a non-linear character of the dependences between the individual factors for describing the dependences between Z<sub>1</sub> = f(X, Y) and Z<sub>2</sub> = f(X, Y), a model on the base of second degree polynomial is chosen.

$$Z_i = b_{0i} + b_{1i}X + b_{2i}Y + b_{12}X.Y + b_{11i}X^2 + b_{22i}Y^2 \quad (4)$$

$i = 1, 2$

and for finding the model coefficients b<sub>i</sub> (i = 0, 1, 2) D – optimum composition plan.

#### *Dependence of sodium hypochlorite current efficiency on the electrolysis time and sodium chloride concentration*

The boundaries of independent factors X /time, h/ and Y /NaCl concentration, C g·dm<sup>-3</sup>/ variation in the development of the mathematical model are chosen as follows:

$$0.5 \text{ h} \leq X \leq 2 \text{ h}, \quad 25 \text{ g} \cdot \text{dm}^{-3} \leq Y \leq 150 \text{ g} \cdot \text{dm}^{-3}$$

Table 1 presents the experiment plan (D - optimum plan).

The model obtained as a result of its fulfillment could be presented by the following equation.

$$CE = 30.87034 - 0.5835 \cdot \tau + 0.6481 \cdot C - 2 \cdot \tau^2 - 0.0017 \cdot C^2 - 0.0283 \cdot \tau \cdot C \quad (5)$$

where CE, % is current efficiency /dependent factor Z/.

The model correlation coefficient r runs to 0.99, which proves its adequacy.

In Fig. 2, where the model is presented in graphic form, it is seen that current efficiencies

grow with the increase in the chloride concentration and maximum values of 70–72% are observed at a concentration range of 100–150 g·dm<sup>-3</sup>.

**Table 1.** Plan of experiment: X, time (h); Y, concentration of NaCl (g·dm<sup>-3</sup>); Z, current efficiency (%).

| X, τ, (h) | Y, C <sub>NaCl</sub> , g·dm <sup>-3</sup> | Z, CE, % |
|-----------|-------------------------------------------|----------|
| 0.5       | 25                                        | 44       |
| 1         | 25                                        | 42       |
| 1.5       | 25                                        | 41       |
| 2         | 25                                        | 35       |
| 0.5       | 50                                        | 58       |
| 1         | 50                                        | 54       |
| 1.5       | 50                                        | 51       |
| 2         | 50                                        | 49       |
| 0.5       | 100                                       | 77       |
| 1         | 100                                       | 76       |
| 1.5       | 100                                       | 67       |
| 2         | 100                                       | 62       |
| 0.5       | 250                                       | 81       |
| 1         | 250                                       | 78       |
| 1.5       | 250                                       | 69       |
| 2         | 250                                       | 64       |

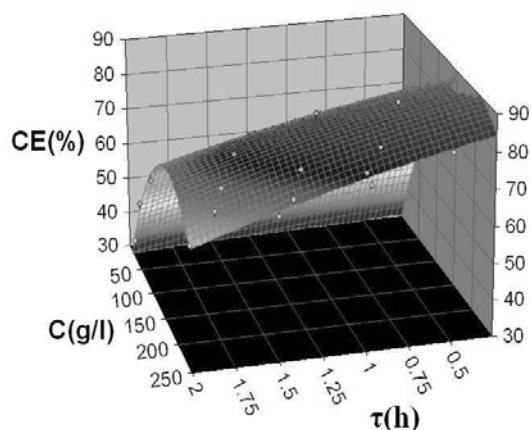


Fig. 2. Dependence of current efficiency CE (%) on time τ (h) and NaCl concentration, C (g·dm<sup>-3</sup>). Current density i = 2.5 A·dm<sup>-2</sup>; anode – graphite.

The fact observed could be explained by acceleration of the chlorine ions oxidation process on account of O<sub>2</sub> release reaction. As mentioned above, O<sub>2</sub> release as a result of water oxidation appears one of the secondary reactions in the hypochlorite production.

The current efficiency increase leads to production of greater hypochlorite quantities. However, as seen in Table 2, with the increase in sodium chloride concentration the conversion coefficient decreases for similar electrolysis time ~ 2 hours.

Thus for instance, in case of chloride concentration change in the range of 25–100 g·dm<sup>-3</sup> the coefficient value decreases nearly 2.5 times. On the basis of these data, a conclusion could be made that in sodium hypochlorite electrosynthesis the optimum concentrations of the charge salt, sodium chloride, are those in the range of 50–100 g·dm<sup>-3</sup>.

**Table 2.** Effect of concentration of NaCl.

| Concentration of NaCl, g·dm <sup>-3</sup> | Active chlorine, mg | Current efficiency, % | Coefficient of conversion, % |
|-------------------------------------------|---------------------|-----------------------|------------------------------|
| 5                                         | 0.6                 | 40                    | 2.54                         |
| 50                                        | 0.78                | 52                    | 1.56                         |
| 100                                       | 1.06                | 70                    | 1.09                         |
| 150                                       | 1.08                | 72                    | 1.06                         |

*Dependence of specific energy consumption on current density and time*

In the development of the model, on the base of preliminary experiments, the following variation range boundaries of the independent factors X (time, τ) and Y (current density *i*, A·dm<sup>-2</sup>) are assumed.

$$0.5 \text{ h} \leq X \leq 2 \text{ h}, \quad 2.5 \text{ A} \cdot \text{dm}^{-2} \leq Y \leq 10 \text{ A} \cdot \text{dm}^{-2}$$

As a result of the experiment plan realization, the following equation is obtained for the dependence of the output factor Z – specific energy consumption /W, Wh·g<sup>-1</sup>/ from the input X and Y – current density *i* and time *t*:

$$W = 0.4620 - 3.3597 \cdot \tau + 2.5333 \cdot i + 0.85 \cdot \tau^2 - 0.13717949 \cdot i^2 + 0.85112426 \cdot \tau \cdot i \quad (6)$$

The calculated correlation coefficient is 0.98, which shows the adequacy of the obtained model.

Figure 3 presents the dependence in a graphic form.

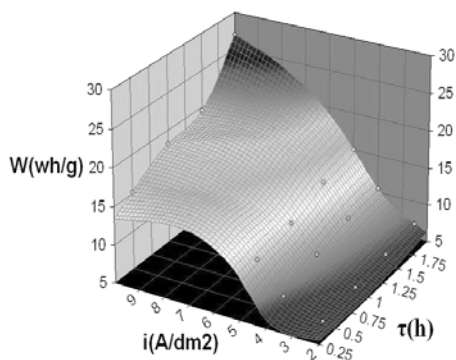


Fig. 3. Dependence of specific energy consumption *W* (Wh·g<sup>-1</sup>) on time *τ* (h) and current density *i* (A·dm<sup>-2</sup>); NaCl concentration – 500 g·dm<sup>-3</sup>, anode – graphite.

It is seen in the Figure, that at high current densities with the advance of the process time maximum values of energy consumption are observed ~ 27 Wh·g<sup>-1</sup>.

The specific energy consumption depends on the electrolysis cell voltage *U* and the current efficiency,  $W = U/q \cdot \Psi$  ( $\Psi$  – current efficiency, *q* – electrochemical equivalent). The subsequent results show that the current efficiency variations with the current density have a maximum, which could be explained by the voltage increase at current density (respectively the intensity) increase.

Table 3 presents the values of different parameters at current density variations in the range of 2.5–10 A·dm<sup>-2</sup>.

**Table 3.** Effect of current density.

| Current density, A·dm <sup>-2</sup> | Energy consumption, Wh·g <sup>-1</sup> | Active chlorine, g | Coefficient of conversion, % | Energy yield, g <sub>ClO<sub>2</sub></sub> ·Wh <sup>-1</sup> |
|-------------------------------------|----------------------------------------|--------------------|------------------------------|--------------------------------------------------------------|
| 2.5                                 | 7.0                                    | 1.5                | 3                            | 0.21                                                         |
| 4.0                                 | 10                                     | 1.7                | 3.4                          | 0.17                                                         |
| 5.0                                 | 15                                     | 1.8                | 3.7                          | 0.12                                                         |
| 10.0                                | 27                                     | 3.0                | 6.0                          | 0.11                                                         |

As seen in case of greater energy consumption higher quantities of sodium hypochlorite are produced and the conversion coefficient has higher values ~6%. However, there is observed a significant, about 2 times, decrease in the energy yield – g<sub>NaClO</sub>·Wh<sup>-1</sup>.

On the basis of the obtained results, a conclusion could be made that the optimum current densities are 4.0–5.0 A·dm<sup>-2</sup> for which the energy consumption grows to a lower degree while the sodium chloride conversion degree and energy yield have acceptable values.

*Dependence of the current efficiency on the current density and time for different anode materials*

Mathematical models are worked out considering the quantitative correlations between the current efficiency, current density and electrolysis time in the NaClO production on platinized titanium anode/Pt/Ti/and anode of cobalt oxide thermally laid on titanium substrate/CoO<sub>x</sub>/Ti/.

For the variations of the independent factors X /time *t*, hours/ and Y /current density *I*, A·dm<sup>-2</sup>/ the following ranges are assumed:

For Pt/Ti

$$0 \text{ h} \leq X \leq 2 \text{ h}, \quad 5.0 \text{ A} \cdot \text{dm}^{-2} \leq Y \leq 15 \text{ A} \cdot \text{dm}^{-2}$$

For CoO<sub>x</sub>/Ti

$$0 \text{ h} \leq X \leq 2 \text{ h}, \quad 1.0 \text{ A} \cdot \text{dm}^{-2} \leq Y \leq 7.5 \text{ A} \cdot \text{dm}^{-2}$$

The obtained models can be presented by the following equations:

$$CE_1 = 69.4525 - 19.4017 \cdot \tau + 1.5812 \cdot i - 2.875 \cdot \tau^2 - 0.1131 \cdot i^2 - 0.2251 \cdot \tau \cdot i \quad (7)$$

$$CE_2 = 61.1625 - 4.88 \cdot \tau + 4.6339 \cdot i - 2.125 \cdot \tau^2 - 0.4906 \cdot i^2 - 2.31 \cdot \tau \cdot i \quad (8)$$

where, CE<sub>1</sub>, CE<sub>2</sub> are the specific energy consumption, for anode Pt-Ti and anode CoO<sub>x</sub>-Ti, respectively.

The calculated correlation coefficients values are 0.98 and 0.96, respectively, which proves their adequacy.

Figures 4 and 5 present the models in a graphic form.

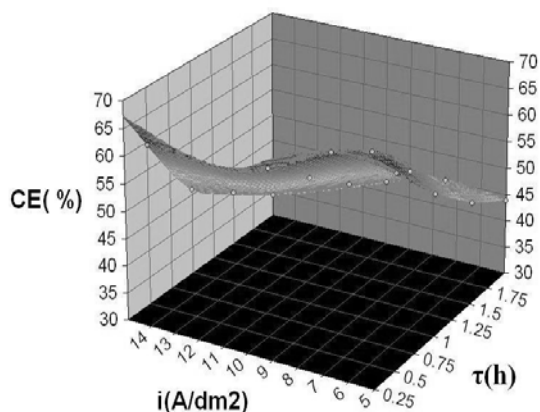


Fig. 4. Dependence of current efficiency (CE %) on time  $\tau$  (h) and current density  $i$  ( $\text{A}\cdot\text{dm}^{-2}$ ); NaCl concentration –  $50 \text{ g}\cdot\text{dm}^{-3}$ , anode – Pt – Ti;

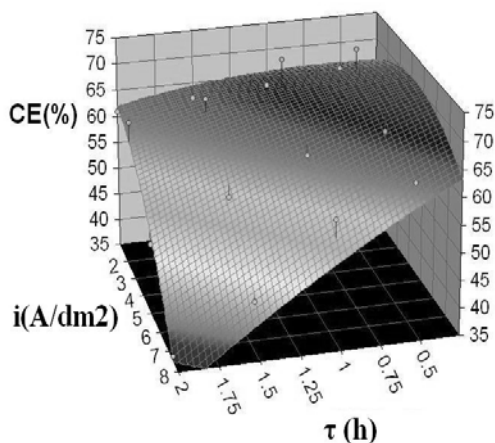


Fig. 5. Dependence of current efficiency (CE %) on time  $\tau$  (h) and current density  $i$  ( $\text{A}\cdot\text{dm}^{-2}$ ); NaCl concentration –  $50 \text{ g}\cdot\text{dm}^{-3}$ , anode –  $\text{CoO}_x$  – Ti;

In Figures 4 and 5 it is seen that the current efficiency values have their maximum at the density variations in the examined ranges. For the Pt/Ti anodes the current efficiency maximum (66–70%) is at current density  $7.5 \text{ A}\cdot\text{dm}^{-2}$  and for the cobalt oxide anode  $\text{CoO}_x/\text{Ti}$  (70–72%) – at  $2.5 \text{ A}\cdot\text{dm}^{-2}$ . The presence of current efficiency maximum is characteristic for insoluble anodes and shows that the hypochlorite production process passes through a diffusion limitation stage. The higher current densities of the Pt/Ti anode maxima are due to the fact that the over voltage of oxygen  $\text{O}_2$  release on the  $\text{CoO}_x/\text{Ti}$  anode exceeds that on the Pt/Ti; as it is known platinum is one of the metals on which oxygen is released with greatest difficulties. The current efficiency maxima on graphite, in accordance with the performed in the present work experiments, have approximately the same values as on the  $\text{CoO}_x/\text{Ti}$  anode, 70–72%, but a lower current density,  $1 \text{ A}\cdot\text{dm}^{-2}$ , corresponds to them. This fact shows the advantages of the platinized titanium

Pt/Ti and the cobalt oxide titanium  $\text{CoO}_x/\text{Ti}$  anodes over the graphite ones, which in addition have short operation life time because of their intensive wear during exploitation.

*Dependence between voltage and inter-electrode space at different current densities in zinc electroextraction*

In the electroextraction process optimization by mathematical modeling as input parameters there are chosen X – current density  $i$ ,  $\text{A}\cdot\text{dm}^{-2}$  and Y – inter-electrode space  $d$ , mm. For output parameter Z we chose the voltage  $U$ , V. The variation ranges of the independent parameters are the following:

$$250 \text{ A}\cdot\text{m}^{-2} \leq X \leq 1000 \text{ A}\cdot\text{m}^{-2},$$

$$20 \text{ mm} \leq Y \leq 80 \text{ mm}$$

On the base of the realization of the optimum plan, a model equation with the following form is worked out:

$$U = 2.4013 + 0.0021 \cdot i + 0.0041 \cdot d - 1.2275 \cdot i^2 - 1.5625 \cdot d^2 + 2.7688 \cdot i \cdot d \quad (9)$$

The model correlation coefficient is 0.99.

It is seen in Fig. 6, presenting the model in a graphic form, that the function has its minimum at current density of  $i = 200 \text{ A}\cdot\text{dm}^{-2}$  and inter-electrode space 20–30 mm. The voltage values for the specified minimum amounts to  $\sim 3.1 \text{ V}$ .

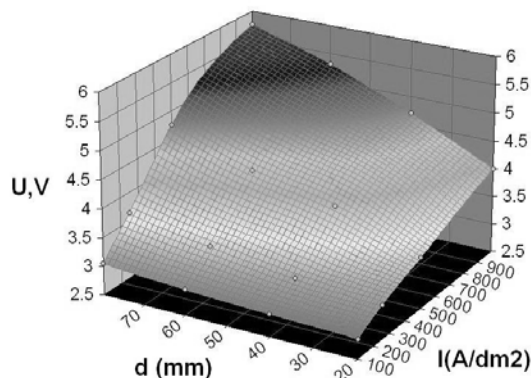


Fig. 6. Dependence of voltage  $U$  (V) on current density  $i$  ( $\text{A}\cdot\text{dm}^{-2}$ ) and inter-electrode space  $d$  (mm) in zinc electroextraction. Solution composition: Zn  $6.5 \text{ g}\cdot\text{dm}^{-3}$ ;  $\text{H}_2\text{SO}_4$   $100 \text{ g}\cdot\text{dm}^{-3}$ ;  $t = 40^\circ\text{C}$ ;

Table 4 presents the distribution of the voltage constituents at  $i = 500 \text{ A}\cdot\text{dm}^{-2}$  and inter-electrode space 20 mm. [18]. As seen in the Table, the anode and cathode potentials carry the greatest relative weight as well as the voltage drop in the electrolyte – 23.5%, 56.1% and 13%, respectively.

As far as the inter-electrode space does not affect the cathode and anode over voltage the dependence of the total voltage is obviously due to the drop increase in the electrolyte that is defined by the

formula  $\Delta U_{\text{electrolyte}} = i.l/\kappa.i$ , where  $i$  – current density,  $\kappa$  – specific electric conductivity,  $l$  – inter electrode space;

**Table 4.** Distribution of voltage constituents in zinc electrolysis.

| Voltage constituents             | V     | %    |
|----------------------------------|-------|------|
| Cathode potential                | 0.82  | 23.5 |
| Anode potential                  | 1.96  | 56.1 |
| Ohm drop in the electrolyte      | 0.45  | 13.0 |
| Ohm drop in conductors of I type | 0.295 | 6.4  |
| total                            | 3.525 | 100  |

However, the current density increase increases both the electrode current over voltage and the solution ohmic drop.

### CONCLUSION

The developed mathematical models, which connect the parameters of NaClO production process and zinc electroextraction, provide possibility to find the conditions for which the current efficiency, voltage and electric energy consumption have optimum values. The high correlation coefficient values  $\geq 0.96$  prove their adequacy.

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## МАТЕМАТИЧЕСКО МОДЕЛИРАНЕ НА ЕЛЕКТРОЛИЗНИ ПРОЦЕСИ

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(Резюме)

Проведена е оптимизация на процесите на електрохимично получаване на натриев хипохлорит и електроекстракция на цинк по метода на математическо моделиране. На базата на уравненията на моделите са установени стойностите на параметрите – плътност на тока, концентрация на компонентите, времетраене, при които са налице максимални добиви по ток, минимално напрежение и специфичен разход на енергия. Показано е, че максимумите на добива по ток  $\sim 70\%$  за анодите от платиниран титан Pt-Ti съответстват на плътности на тока  $7.5 \text{ A}\cdot\text{dm}^{-2}$ , а за кобалтово-оксидните аноди  $\text{CoO}_x\text{-Ti}$ ,  $75\%$ , на плътности на тока  $2.5 \text{ A}\cdot\text{dm}^{-2}$ . Най-високи стойности на коефициентите на превръщане ( $2.54\%$ ) са налице при ниски концентрации на натриев хлорид  $\sim 25 \text{ g}\cdot\text{dm}^{-3}$ . При увеличаването на плътностите на тока до  $10 \text{ A}\cdot\text{dm}^{-2}$  коефициентът на конверсия може да нарасне до  $6\%$ , но това води до значително нарастване на разхода на енергия –  $25 \text{ Wh}\cdot\text{g}^{-1}$ .

При електроекстракцията на цинк най-ниско напрежение  $\sim 3.1 \text{ V}$  е налице при плътности на тока  $i = 200\text{--}300 \text{ A}\cdot\text{m}^{-2}$  и разстояние между разноименните електроди  $20\text{--}30 \text{ mm}$ .